

# Piezo-tuned nonplanar ring oscillator with GHz range and 100 kHz bandwidth

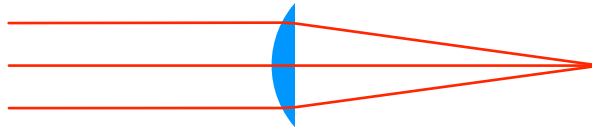
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*KANE OE*



Avo Photonics

Presented at Photonics West, Jan 26, 2022

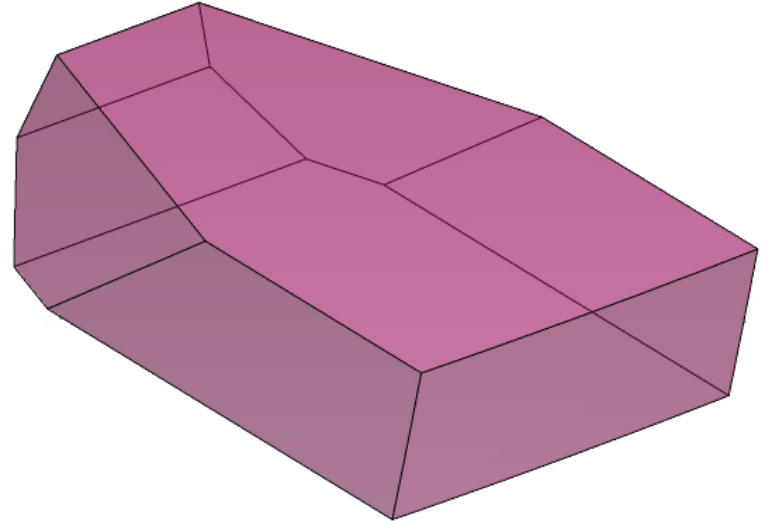
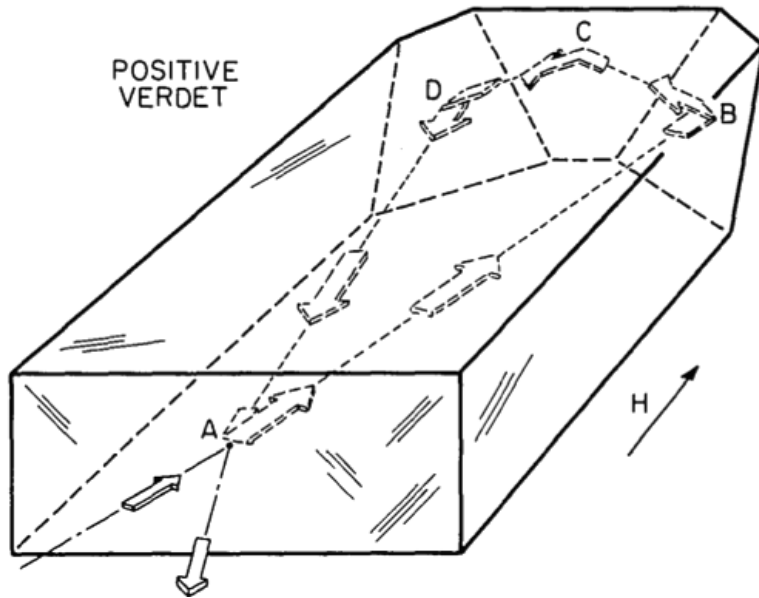
# The “Nonplanar Ring Oscillator” (NPRO)

February 1985 / Vol. 10, No. 2 / OPTICS LETTERS

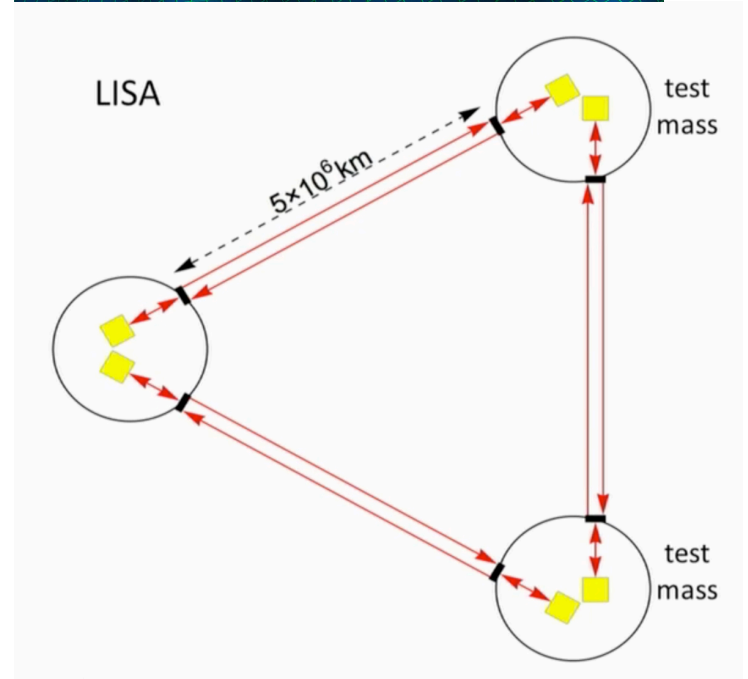
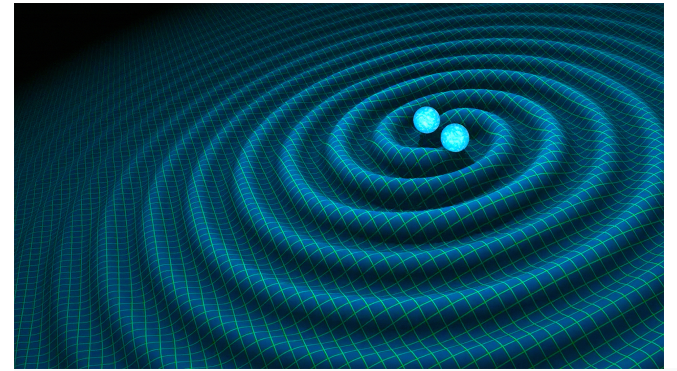
## Monolithic, unidirectional single-mode Nd:YAG ring laser

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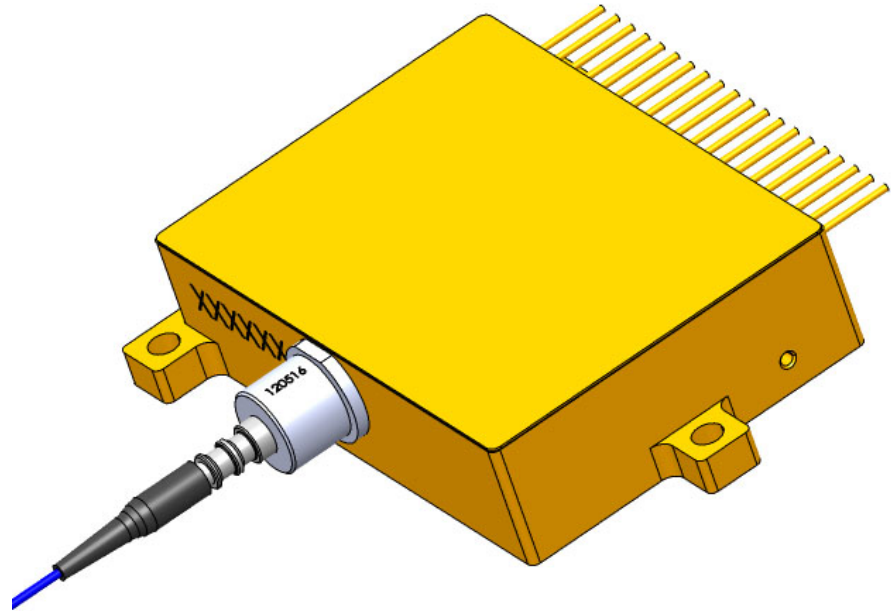


# Gravitational Wave Detection



# NASA Goddard / AVO / Kane collaboration

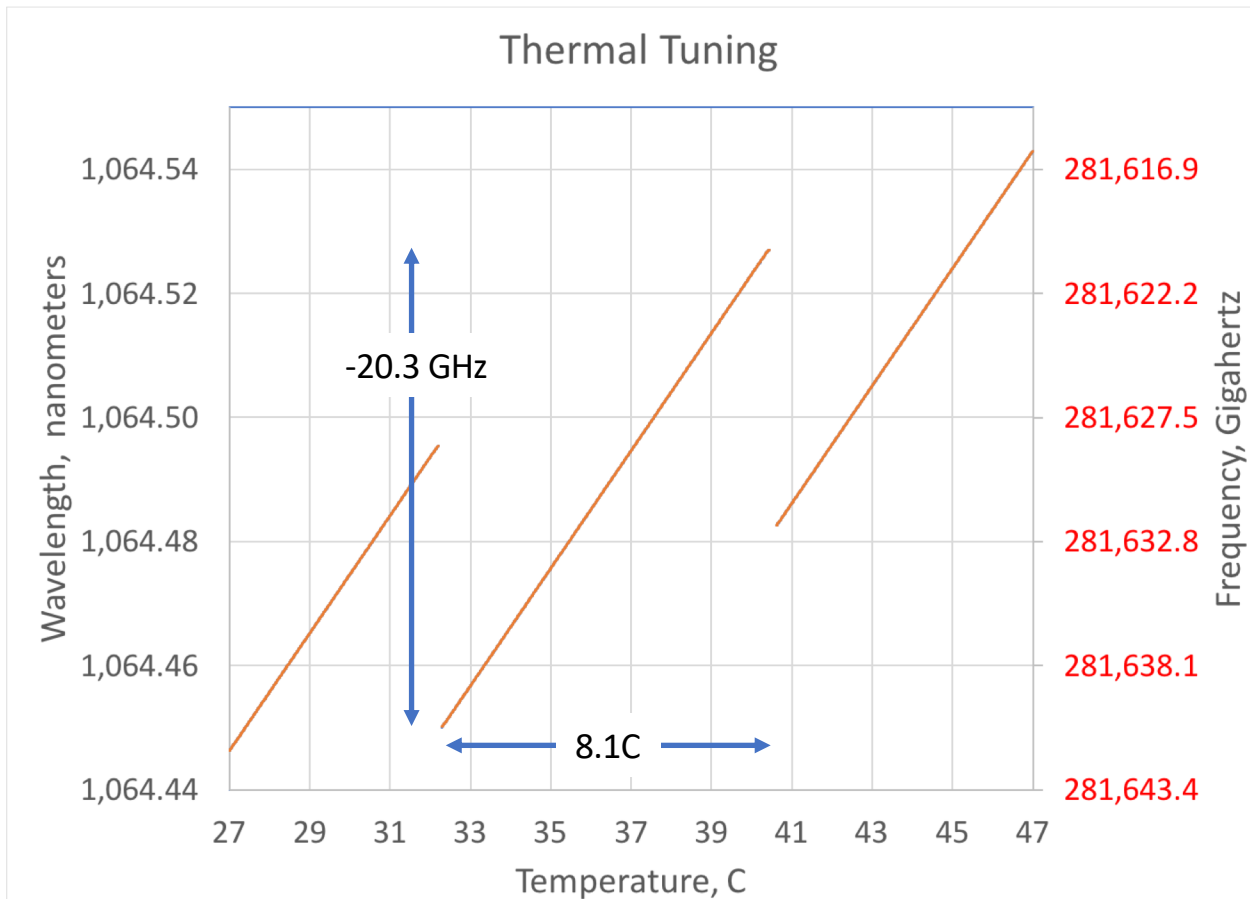
- “ $\mu$ NPRO”
- Welded PM single-mode fiber coupling
- Dual polarization-combined pump lasers
- 700 mW @ 1064 nm
  - 10X what LISA needs to saturate YDFA Stage 1



*58 x 41 x 14 mm*

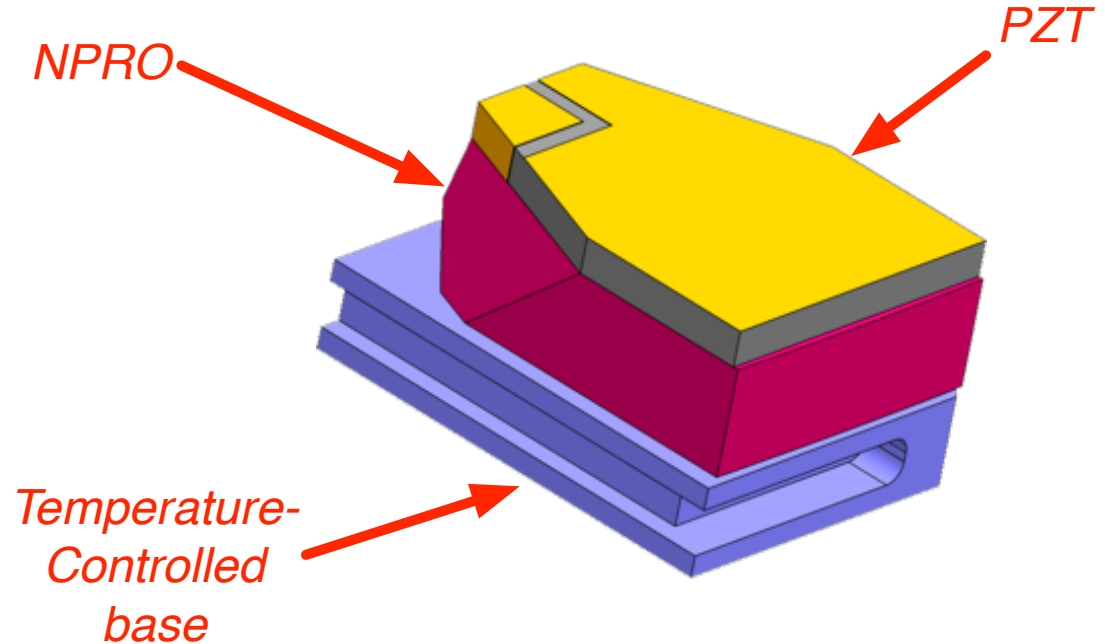
# NPROs are Tunable – Thermal: Slow, Wide Range

$$\frac{\Delta\lambda}{\lambda} = \frac{\Delta\text{optical path length}}{\text{optical path length}} \approx \frac{-\Delta f}{f}$$



# Strain tuning – fast, narrower range

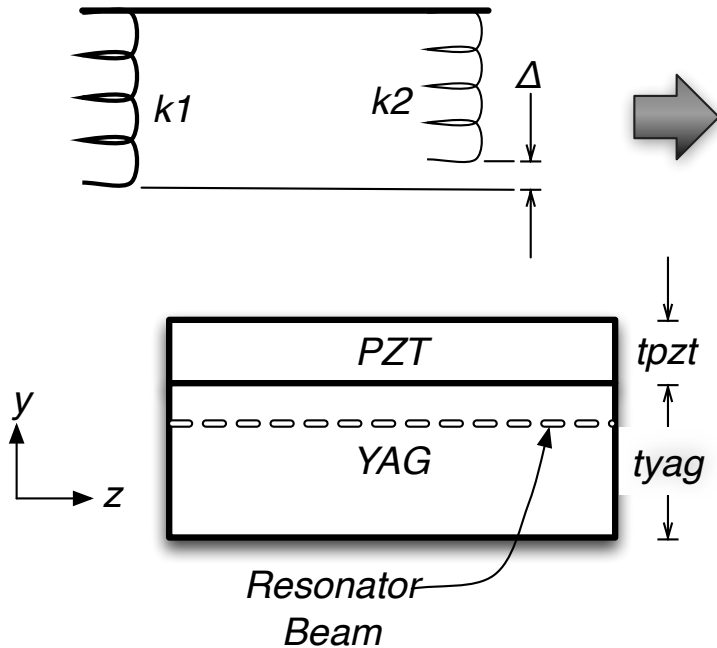
- “Prior art” response:
  - 1 MHz/Volt
- ESA Requirement for LISA
  - $\pm 100$  MHz
- NASA Goal
  - $\pm 12$  volt drive
  - $> 8.33$  MHz/volt



# Demonstrated: 18.2 MHz/Volt

- Design changes:
  - Make the NPRO small. With proportions maintained, the MHz/volt coefficient scales inversely with linear dimension
  - Maximize the product of the Young's Modulus  $Y$  and the charge constant  $d_{31}$  of the PZT material
  - Make the internal beam as near as possible to the PZT
  - Make the PZT is thin as practical

# Simple-minded Calculation: Uniform Strain



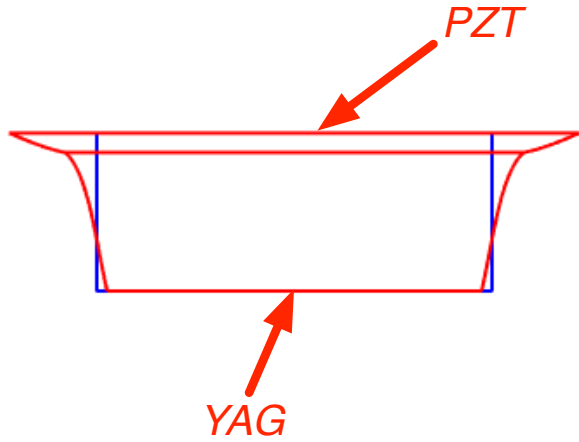
*Simple 2-spring  
"lumped element"  
model*

$$\text{Tuning coefficient} = \frac{f Y_{\text{PZT}} d_{31}}{(Y_{\text{YAG}} t_{\text{YAG}} + Y_{\text{PZT}} t_{\text{PZT}})}$$

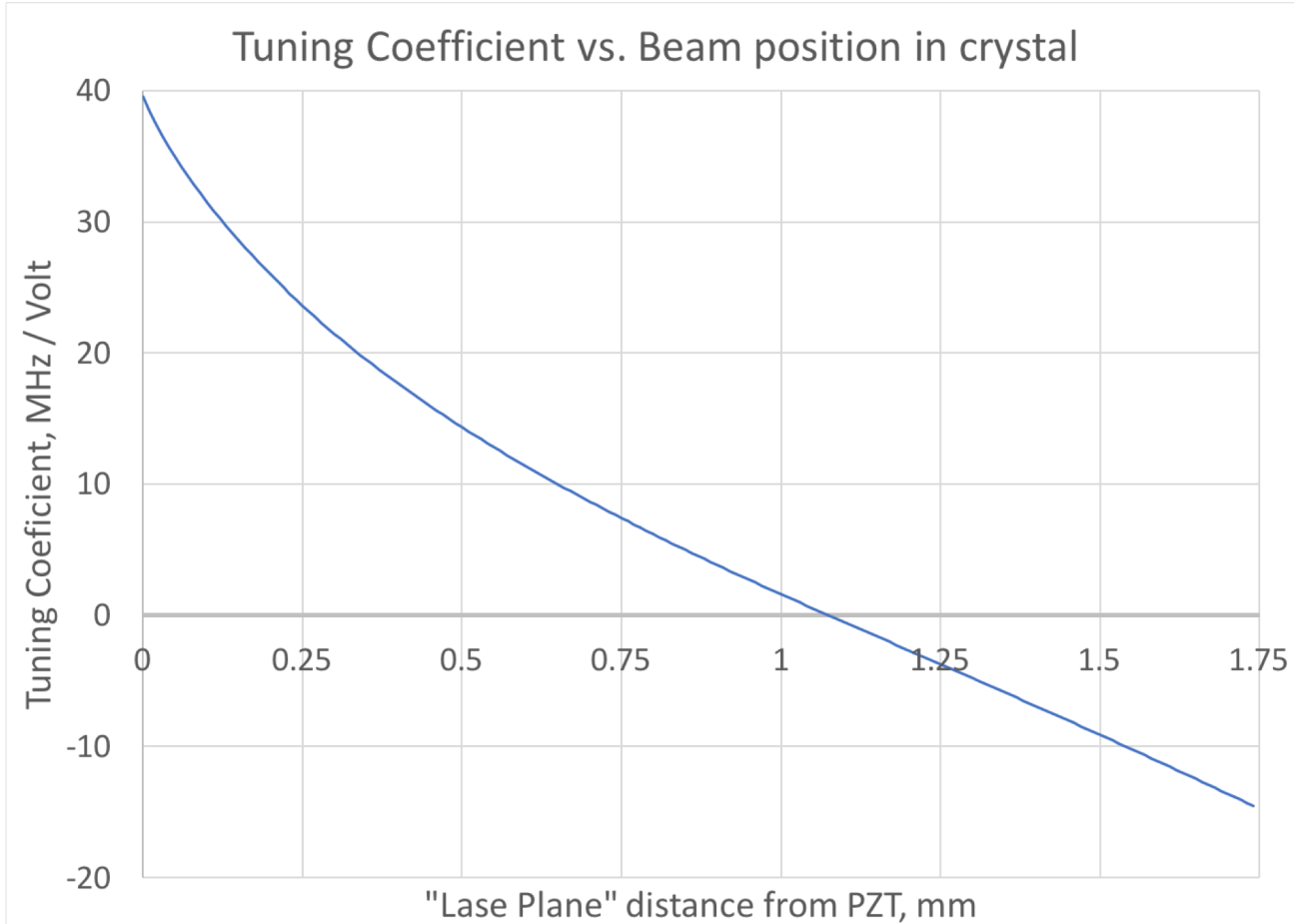
- 3 predictions
  - Figure of Merit for PZT
    - $Y d_{31}$
  - Inverse Linear scaling
  - Thin PZT beneficial, to a point
- For  $\mu\text{NPRO}$  parameters
  - 14.3 MHz/volt
- *This neglects the elasto-optic effect*



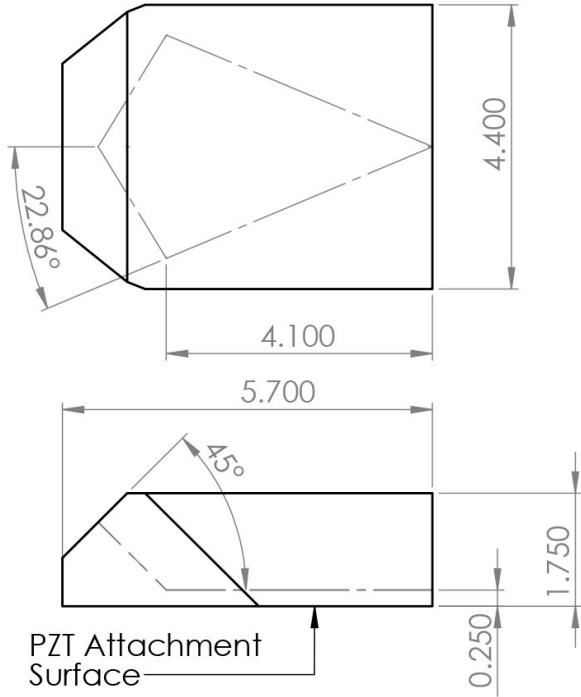
# Effect of non-uniform strain



*2-dimensional numerical solution*



# μNPRO Fabrication

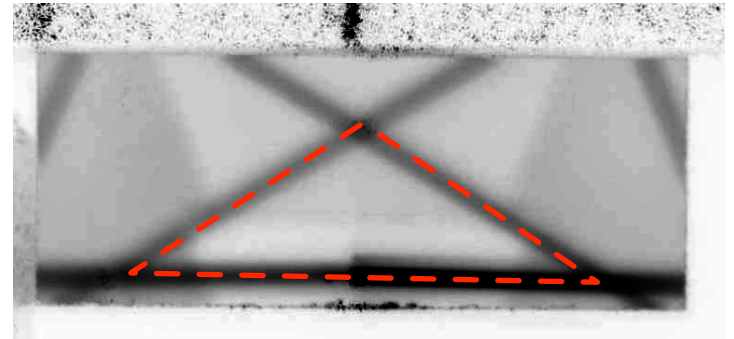


Controlling Dimensions	
AOI on front face	22.86°
Out-of-plane angle	45°
AOI on back face	49.34°
Altitude of base triangle	4.1 mm
Lase plane	0.25 mm
Length	5.7 mm
Width	4.4 mm
Thickness	1.75 mm
Derived Dimensions	
AOI on side face	48.73°
Round trip distance	13.456 mm

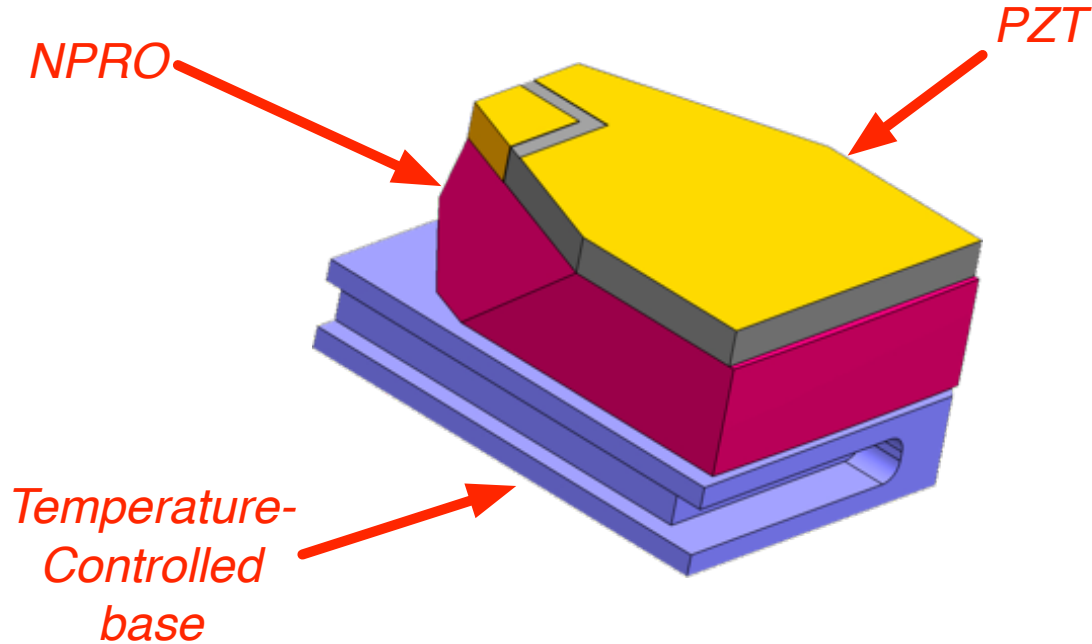
*Control of beam position demonstrated*

μNPRO Fab	# tested	Average (0.25 mm by design)	Standard Deviation
#1	7	0.26 mm	0.02 mm
#2	62	0.20 mm	0.06 mm
#3	4	0.24 mm	0.03 mm

*View looking into front face of μNPRO while lasing, negative image*



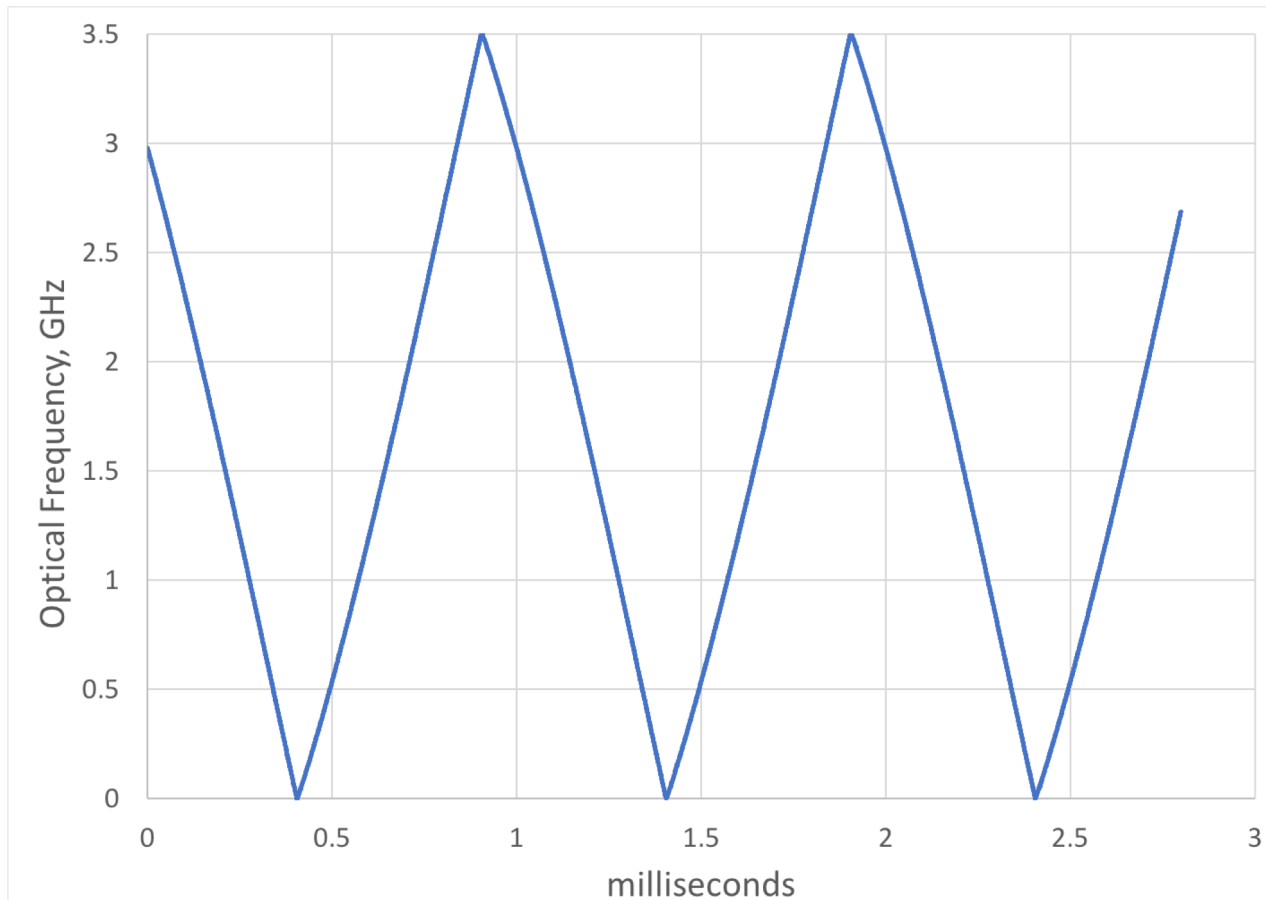
# PZT Material



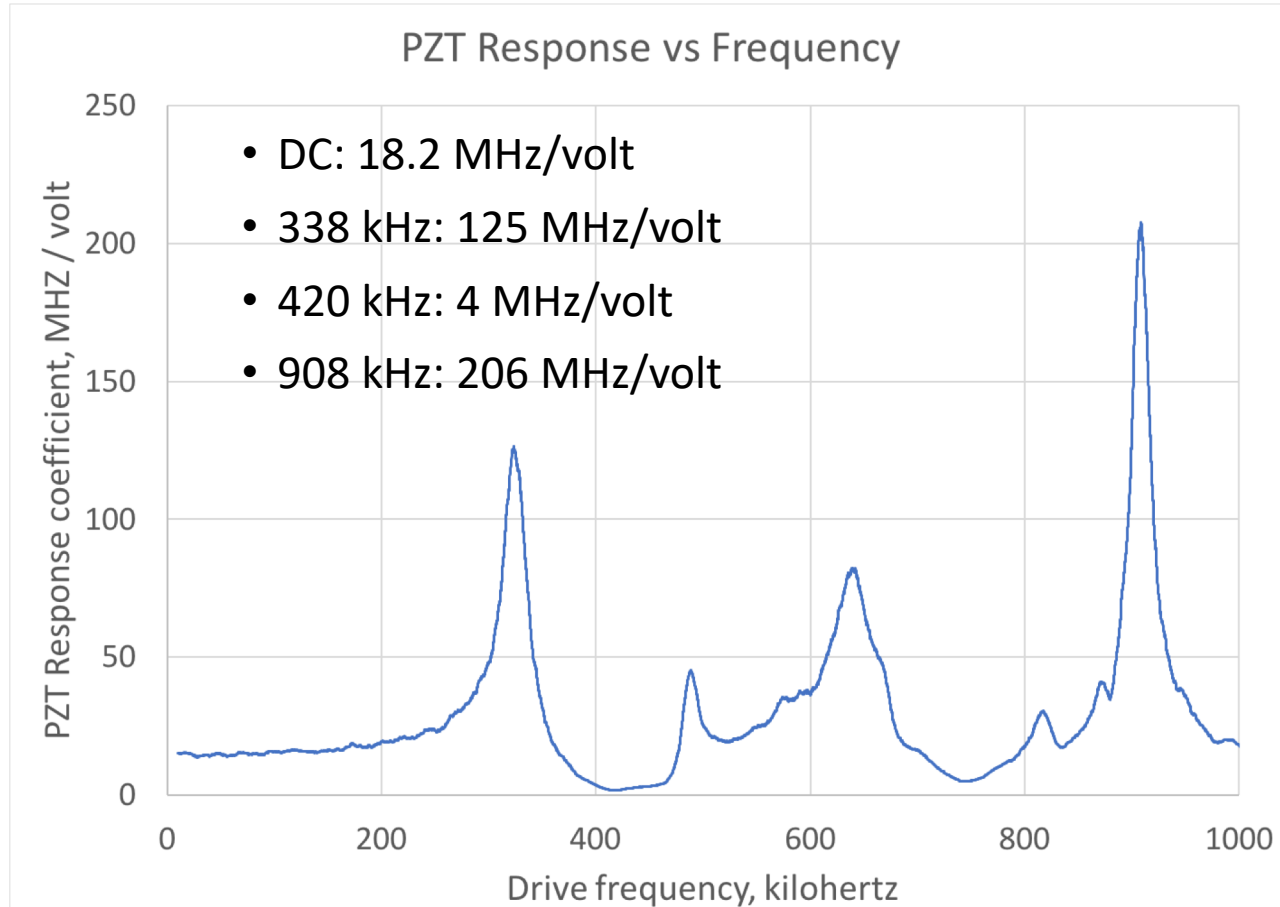
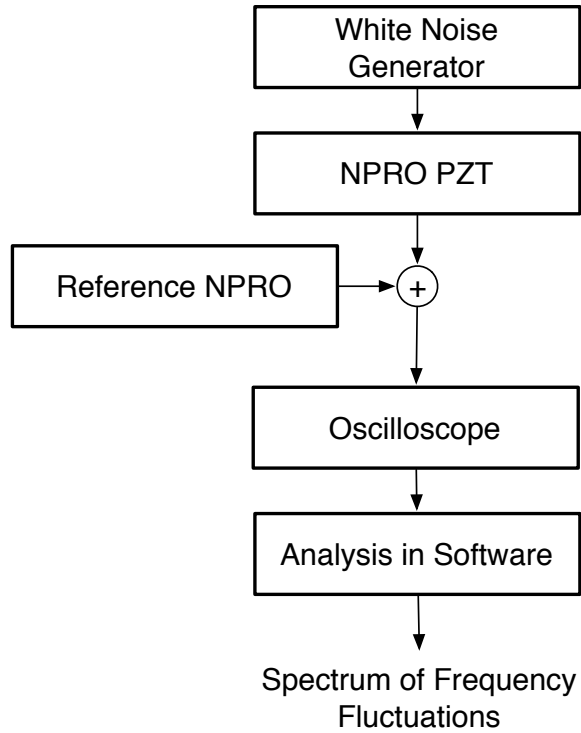
- 3265HD available from CTS Corporation
  - $Y_{11}^E = 69$  Gpa
  - $d_{31} = -370$  pm/volt
- 0.25 mm thick
- Max safe voltage  $\pm 125$  volts

# Performance driven by 192 volts, peak-peak

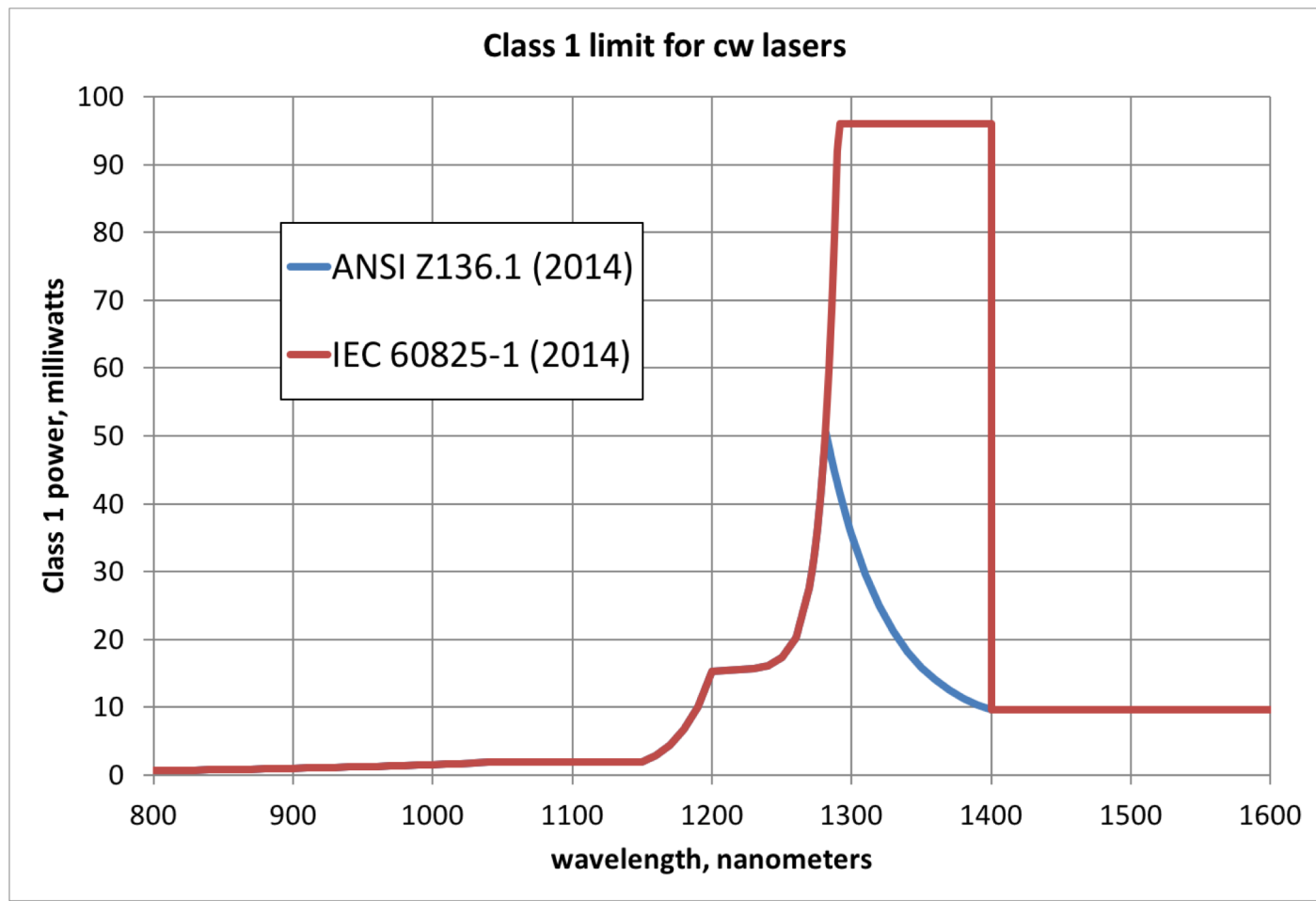
- 1 kHz triangle
  - $\pm 96$  volts
- 3.5 GHz peak-peak
- 18.2 MHz/volt
- Beat-note measurement



# Bandwidth of response limited by resonances

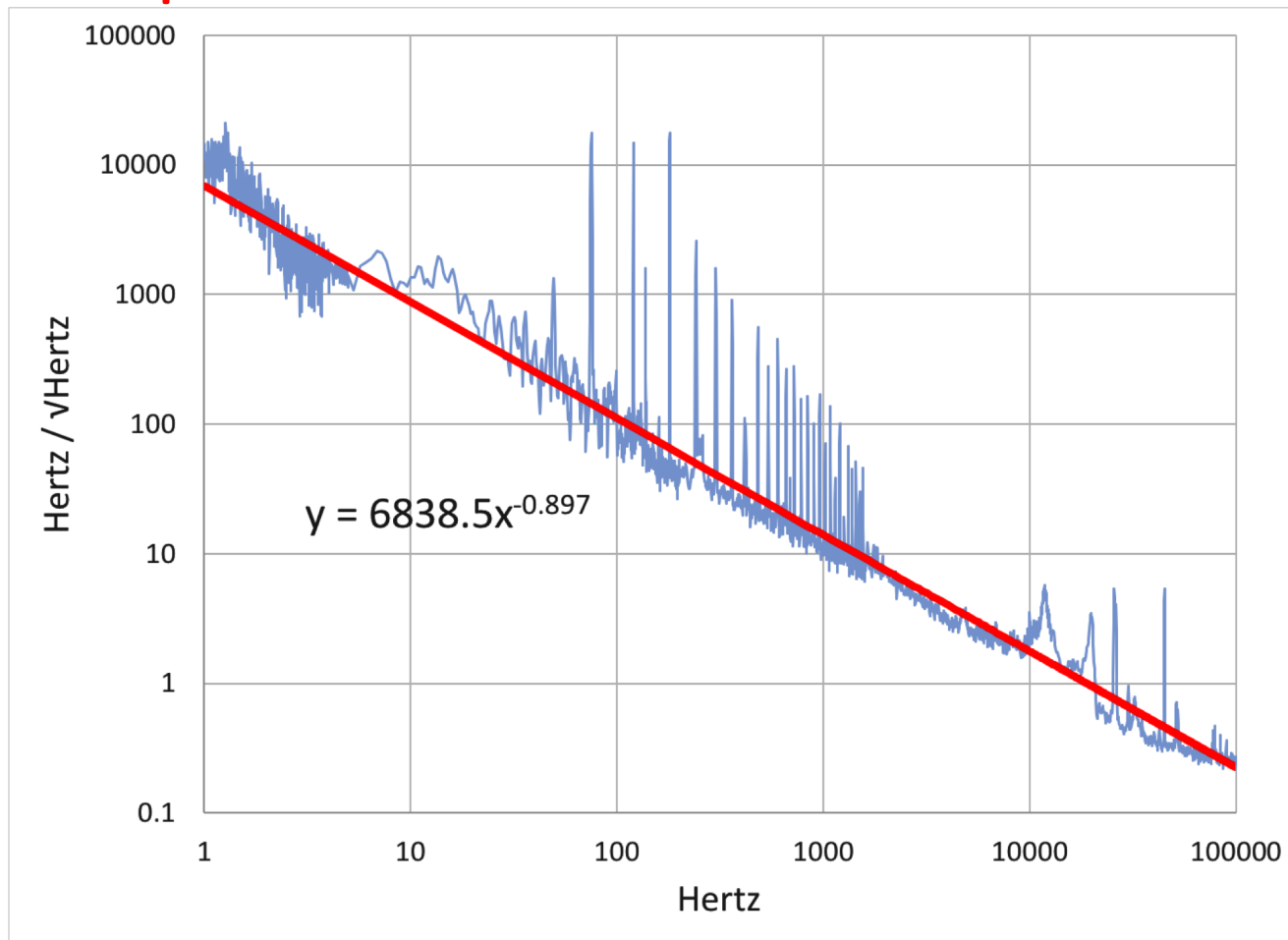


# FMCW LIDAR? 1319 nm best $\lambda$ for eye-safety



# Unsurpassed low phase noise of NPRO

- NASA tested competing designs, NPRO best for LISA
- Sub-kHz linewidth
- 1/f spectrum



# Conclusion

- High Power (~watt)
- Narrow linewidth (kHz)
- Broad and fast tunability
  - GHz per  $\mu\text{sec}$
- Two standard wavelengths
  - 1064 nm – can amplify to 100 watts
  - 1319 nm – best eye-safety
- With proper tooling, fab cost is dominated by Nd:YAG raw material
- Further progress is possible – please challenge me!

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